6th ECCOMAS Conference on Smart Structures and Materials SMART2013 - Politecnico di Torino, 24-26 June 2013 www.smart2013.com

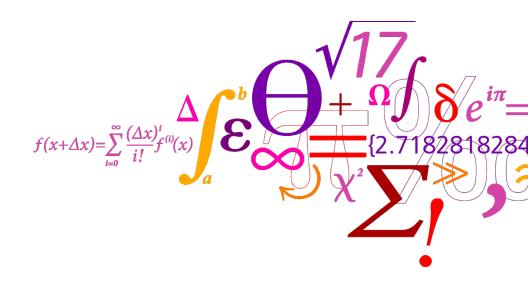


Design and manufacturing of a morphing flap for wind turbine blades

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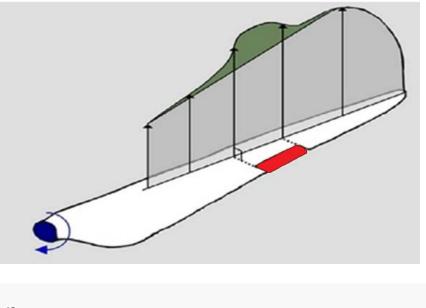


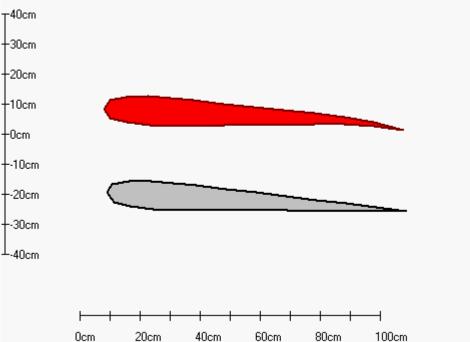




Background

- Designs and prototypes
- □ Summary





Past:



The pitch system enabled the wind turbine to actively regulate loads (full blade)

Our hope: The flap system will open up new blade designs for wind turbine application (local flow control)

Numerical studies have indicated that the flap system have significant load reduction potential



article	c_f [%]	dr_f/r [%]	$\delta [\pm^{\circ}]$	T.I. [%]	shear exp. [-]	V_{av} [m/s]	reduction in std of RBM [%	reduction in DEL [%]	controller
Riziotis et al. 2008	10	15-47	6	-	0.2	8, 12, 16	30-35 (range)	,-	PID
Andersen et al. 2008	10	63	8	14-18	0.14	7, 11, 18	-	36.2-47.9	HPF+inflow
Lackner et al. 2009	10	20	10	NTM, ETM	0.2	8, 12, 16, 20	-	5.6-24.6	PID
Barlas et al. 2009	10	20	10	NTM	0.2	8, 11.4, 16	5.7-22.4	-	PID
Andersen et al. 2009	10	15-30	8	-	11.4	-	-	25-37	HPF
Resor et al. 2010	10	24	10	6	0.2	15	26-30.9	27-31.3	PD, HPF+note
Wilson et al. 2010	10	24	10	6	0.2	15	13.3	15.5	LQR
Berg et al. 2010	10	25	10	6	0.2	15	8.7-18.1	10.9-17	PD, LQR
this article	10	18	8	6, NTM	0.2	7, 11.4, 15	10.9-30.7	10.9-27.3	MPC+inflow

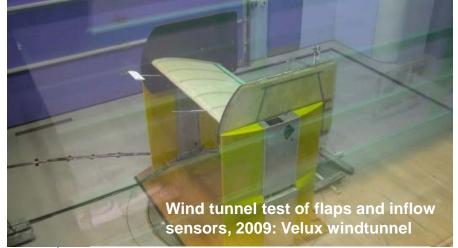
Barlas, Thanasis; Van Der Veen, Gijs; van Kuik, Gijs; Model Predictive Control for wind turbines with distributed active flaps: Incorporating inflow signals and actuator constraints. Article first published online: 17 NOV 2011 DOI: 10.1002/we.503

Wind tunnel experiments have shown that the flap system can reduce blade loads



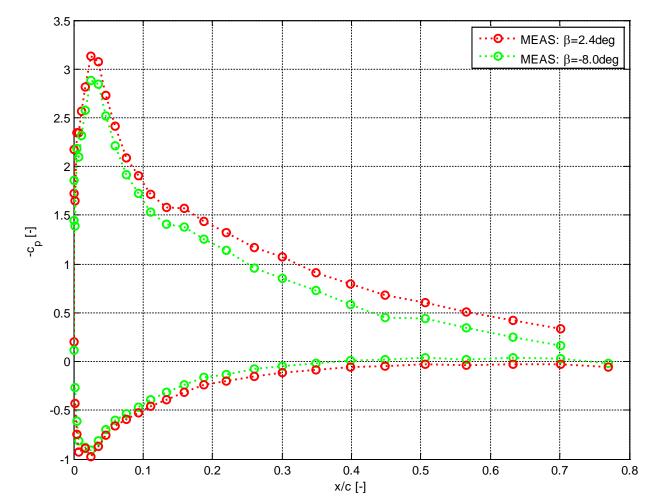






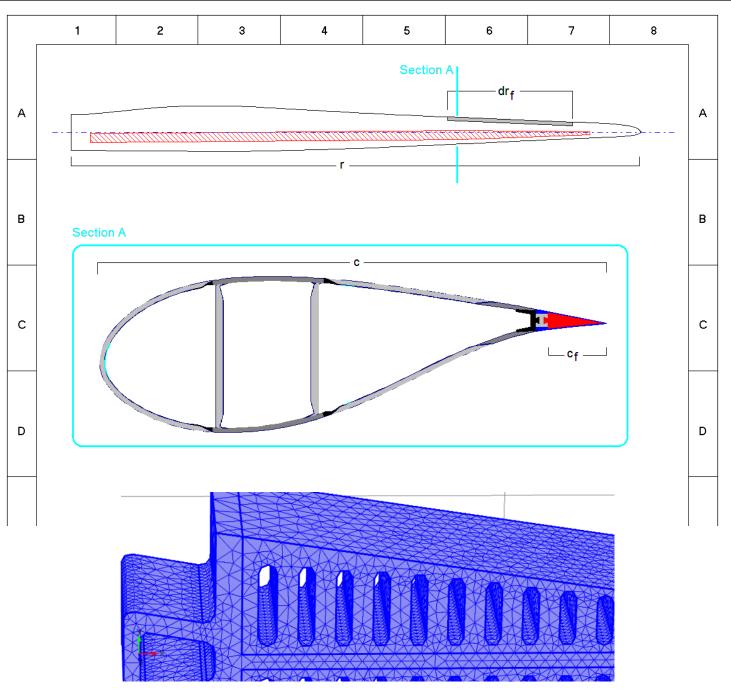
Wind tunnel experiments have shown that the flap system can reduce blade loads





AOA=8deg

The flap system will affect many levels of todays blade design

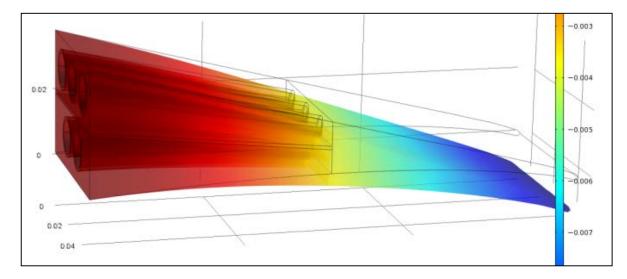


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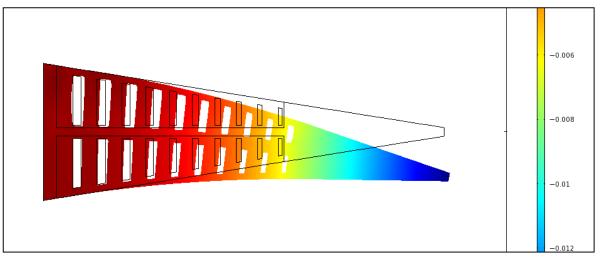
Focus: the

flap design





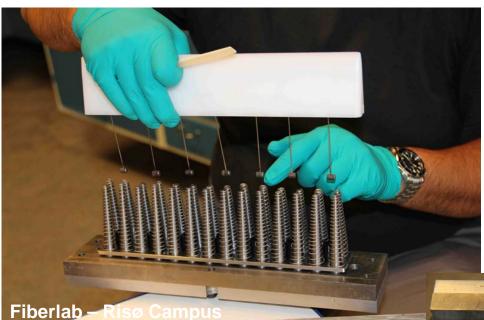
CHORDWISE CAVITIES FOR MOULD MANUFACTORING

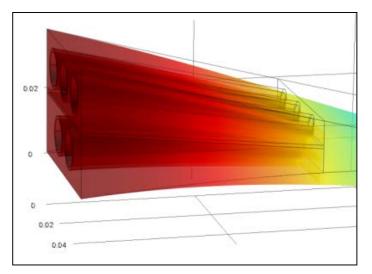


SPANWISE CAVITIES FOR EXTRUSION

Chordwise cavities for mould manufactoring





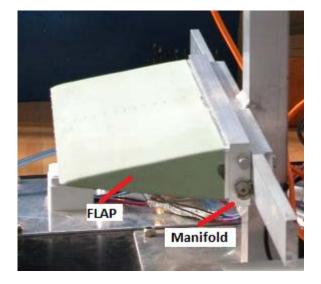


Cavities had to be reinforced in order to maintain deflection characteristics



Chordwise cavities for mould manufactoring



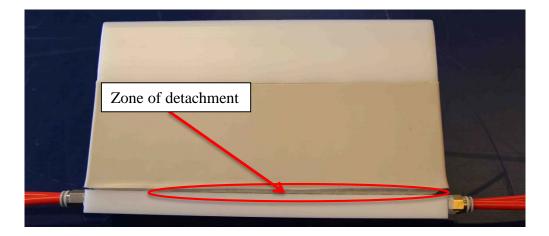


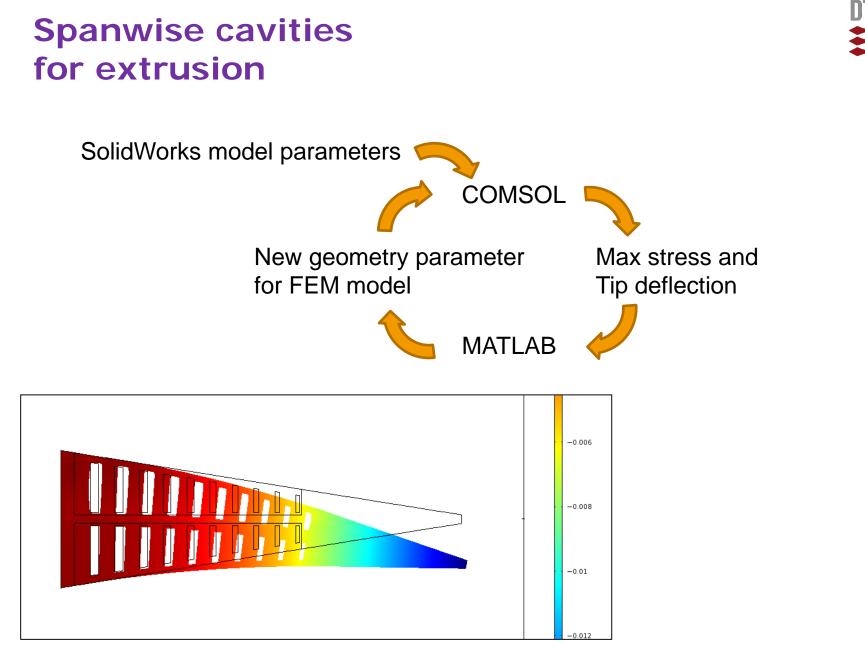
Large surface contact area for both hydraulic and pneumatics solutions



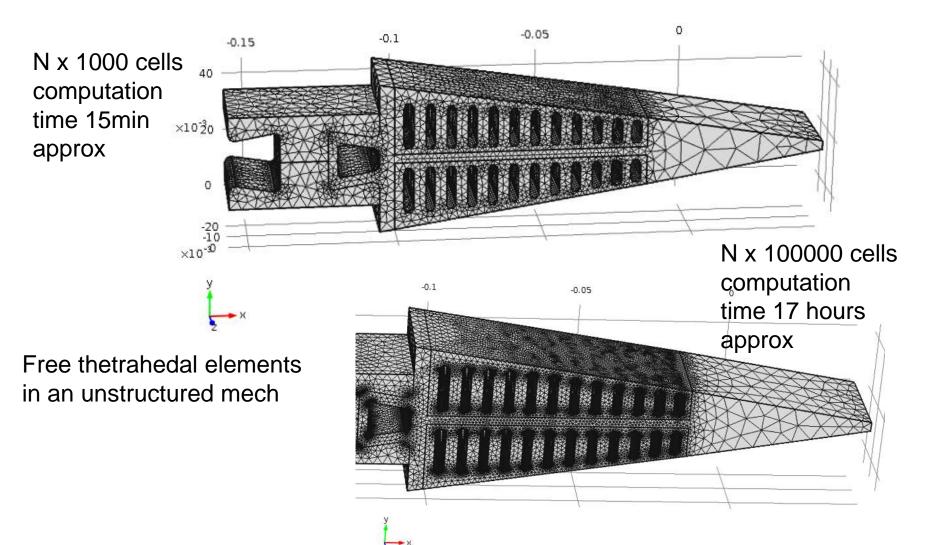
"Development of the controllable rubber trailing edge flap technology for MW turbines". Advances in Wind Turbine Rotor Blades, 13 -

Zone of detachment problem

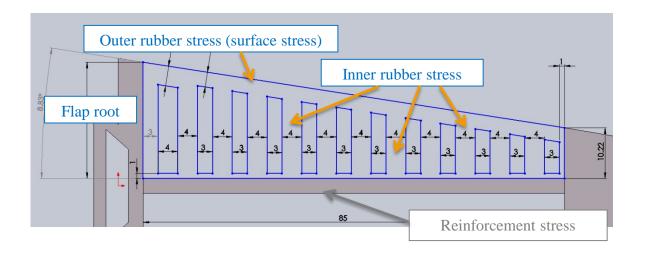










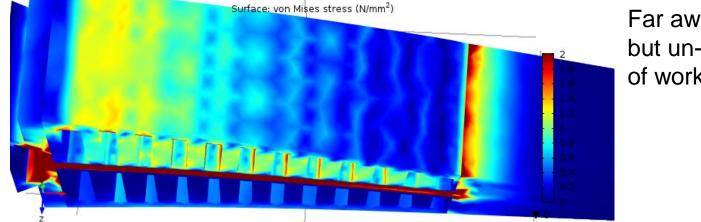


Cavity pressures investigated for 1,2,3,4,5,6,7 and 8 bar overpressure

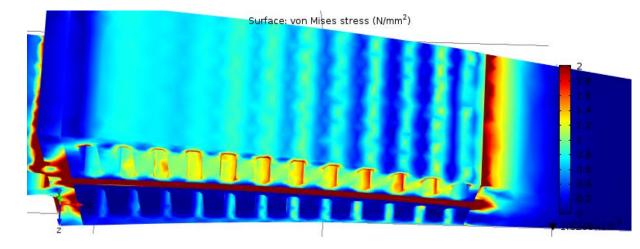
Santoprene 101-73 thermoplastic vulcanizate Wacker 4670 silicon

Target: maximum stress' for the rubber flap part at 15% elongation is 8MPa

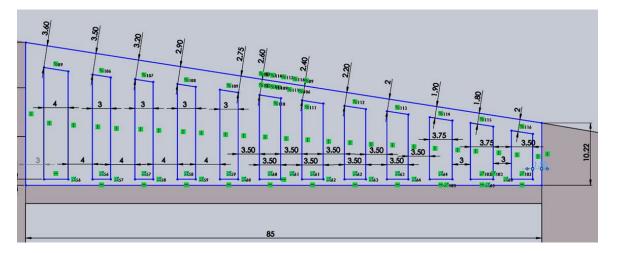




Far away from 8MPa but un-even distribution of work load



Here the full surface is at work causing a more even flap deflection





Sharp edges

Rounded edges



Pressure Obar: von Mises stress (N/mm²) -0.1 -0.05 0 40 20 ×10⁻³ 0 -200 **V** 0 **A** 0 ×10⁻³ 0.5 1.5 2.5 3.5 4 4.5 2 1 3

Numerical results

				Rubber		Reinforcement		
		Flap deflection		outer	Inner	w/ part.	inner	w/ part.
Cavity	pressure	angle	displa.	Stress	Stress	safty fac.	stress	saf. fac.
design	bar	deg	mm	N/mm ²				
Rounded	4	4.2	11.0		1.7	2.3 (3.48)	8	11
old square	6	6.6	17.4	3.2	4.1	5.5 (1.45)	12	16
Square	6	6.8	17.8	2.5	4.0	5.4 (1.48)	12	16
Rounded	6	6.5	17.1	2.4	2.6	3.5 (2.29)	12	16
old square	8	8.3	21.9		6.1	8.2 (0.97)	14	19
Square	8	8.9	23.5		6.0	8.1 (0.99)	14	19
Rounded	8	9.1	23.9		4.1	5.5 (1.45)	14	19

Conclusion

The new spanwise cavity design lowers the critical stresses. (8.2MPa -> 5.5MPa for 8bar overpressure w/ 1.35 saftyfactor) (5.5MPa -> 3.5MPa for 6bar overpressure w/ 1.35 saftyfactor)

Compared to the original design the flap deflection angles remain almost the same.

According to the FEM models used it is recommended to use round edges instead of sharp edges for the cavities

Future...



Thank you for your attention!

